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# Approximate Analytical Study of Fingero-Imbibition Phenomena of Time-Fractional Type in Double Phase Flow through Porous Media

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**Abstract.** We consider the non-linear partial differential equation of time-fractional type describing the spontaneous imbibition of water by an oil-saturated rock (double phase flow through porous media). The fact that oil and water form two immiscible liquid phases and water represents preferentially wetting phase are the basic assumption of this work. The Homotopy Analysis Method is used to obtain the saturation of injected water. We obtain the graphical representation of solution using MATLAB *R*2007*b* and Microsoft Excel 2010 with different fractional order ( $\alpha > 0$ ) and the comparison is made with the solution obtained in [19] using Adomian Decomposition Method when  $\alpha = 1$  including numerical values.

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Key Words and Phrases: Fractional derivative, Fingero-imbibition, Double phase flow in porous media, Immiscible fluid, Homotopy Analysis Method

## 1. Introduction

In Caputo [6] and He [10], the approach used to account for the effects of changing flux is to embody the effects of memory which has to do with posing problem in terms of fractional calculus. Levy-flight type of transport is a well known diffusion process which is described by a fractional system. Motivated by this idea, we propose a fractional type Fingero-Imbibition phenomena equation in double phase flow through porous media and obtain analytical approximate solution using Homotopy Analysis Method, HAM. We consider equation of form

$${}^{C}D_{T}^{\alpha}S(X,T) = \left(\frac{\partial S(X,T)}{\partial X}\right)^{2} + S(X,T)\frac{\partial^{2}S(X,T)}{\partial X^{2}}$$

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where  ${}^{C}D_{T}^{\alpha}$  is the Caputo fractional derivative with appropriate initial condition.

When there is difference in the viscosity of two flowing phases due to wetting difference, then we have fingering phenomena. The importance of this phenomenon has gained attention by various concerned fields such as geophysics, geo-hydrology, reservoir engineering etc, with little or no attention to the fractional type.

Generally, for the past three decades, fractional calculus has been considered with great importance due to its various applications in fluid flow, control theory of dynamical systems, chemical physics, electrical networks, and so on. The quest of getting accurate methods for solving resulted non-linear model involving fractional order is of almost concern of many researchers in this field today.

Various methods have been put to use successfully to obtain analytical solutions such as Adomian Decomposition Method (ADM) [2, 19, 20], Variational Iteration Method (VIM) [11, 20], Homotopy Perturbation Method (HPM) [9], and EXP-function Method [24] see also [12–14, 23]. One of the powerful analytical approach to solving non-linear differential equations is Homotopy Analysis Method (HAM) [1, 4]. Recent works have been done using this method (HAM) to obtain analytical solutions of some differential equations given improvement on the method [3, 5, 7]. Xu *et al.* [25] recently applied the HAM to linear, homogeneous one and two dimensional fractional heat-like PDEs subject to the Neumann boundary conditions. Very recently, HAM was shown to be capable of solving both linear and non-linear systems of fractional partial differential equations [15].

This paper considers equation (1) subject to some appropriate initial where  ${}^{C}D_{T}^{\alpha}(\cdot) = \frac{\partial^{\alpha}(.)}{\partial T^{\alpha}}$  is a Caputo fractional differential operator. We compare the result obtained by HAM with that of ADM [19], when  $\alpha = 1$  to affirm the reliability of the method including numerical values. We obtain numerical results at the end with different values of  $\alpha$  and h (h is auxiliary parameter introduced in HAM) given the effect of both parameters on solution of fingero-imbibition phenomena of fractional type in double phase flow through porous media.

## 2. Preliminaries

Here we state necessary tools to the actualization of the aim of this paper including definitions and some known results. This work adopts Caputo's definition to some concepts of fractional derivatives which is a modification of the Riemann-Liouville's definition and has the advantage of dealing properly with initial value problems. The initial conditions are given in terms of the field variables and their integer order which is the case in many physical processes.

**Definition 1.** A real function *l* is said to be in the space  $C_{\mu}$ ,  $\mu \in \mathbb{R}$ , x > 0, if there exists a real number  $p(>\mu)$  such that

$$l(x) = x^p l_1(x),$$

where  $l_1 \in C[0, \infty)$  and it is said to be in the space  $C^m_\mu$  if and only if  $l^{(m)} \in C_\mu$ ,  $m \in \mathbb{N}$ .

**Definition 2.** The Riemann-Liouville's (RL) fractional integral operator of order  $0 < \alpha < 1$ , of a

function  $f \in L^1(a, b)$  is given as

$$J^{\alpha}f(t) = \frac{1}{\Gamma(\alpha)} \int_{0}^{t} (t-\tau)^{\alpha-1} f(\tau) d\tau, \ t > 0,$$
(2)

where  $\Gamma$  is the Gamma function and  $J^0 f(t) = f(t)$ .

**Definition 3.** The Riemann-Liouville's (RL) fractional derivative of order  $0 < \alpha < 1$ , of a function f is

$$D_{0_{+}}^{a}f(t) = DJ_{0^{+}}^{1-a}f(t).$$
(3)

provided the right-hand side exists where D = d/dt.

Definition 4. The fractional derivative in the Caputo's sense is defined as [21],

$${}^{C}D^{\alpha}f(t) = J^{n-\alpha}D^{n}f(t) = \frac{1}{\Gamma(n-\alpha)} \int_{0}^{t} (t-\tau)^{n-\alpha-1}f^{(n)}(\tau)d\tau,$$
(4)

where  $n-1 < \alpha \leq n, n \in \mathbb{N}, t > 0$ .

Caputo's fractional derivative also has a useful property [8]

$$J^{\alpha C} D^{\alpha} f(t) = f(t) - \sum_{k=0}^{n-1} f^{(k)}(0^{+}) \frac{t^{k}}{k!},$$
(5)

where  $n - 1 < \alpha \le n$ .

**Lemma 1.** Let  $\alpha \ge 0$ ,  $\beta \ge 0$  and  $f \in CL(a, b)$ . Then

$$J_a^{\alpha} J^{\beta} f(t) = J_a^{\alpha+\beta} f(t), \tag{6}$$

for all  $t \in (a, b]$ .

**Lemma 2.** Let  $t \in (a, b]$ . Then

$$\left[J_a^{\alpha}(t-a)^{\beta}\right](t) = \frac{\Gamma(\beta+1)}{\Gamma(\beta+\alpha+1)}(t-a)^{\beta+\alpha}, \qquad \alpha \ge 0, \ \beta > 0.$$
(7)

**Remark 1.** From the definitions given above, we observed that the Riemann-Liouville fractional derivative of a constant function is not equal to zero while that of Caputo fractional derivative of constant function is zero.

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## 3. Method of Solution

Consider a non-linear fractional partial differential equation of the form

$$\begin{cases} D_t^{\alpha}(f(x,t)) = A(f, f_x, f_{xx}) + B(f, f_x, f_{xx}) + C(x,t) & n-1 < \alpha \le n, \ t > 0\\ f^{(k)}(x,0) = g_k(x) & k = 0, 1, 2, 3, \dots, n-1, \end{cases}$$
(8)

where *A* is a linear operator and *B* is a non-linear operator both of which might include other fractional derivatives of order less than  $\alpha$  and *C* is a known analytic function.

Using (5), we obtain

$$f(x,t) = \sum_{k=0}^{n-1} g_k(x) \frac{t^k}{k!} + J^{\alpha} C(x,t) + J^{\alpha} A(f,f_x,f_{xx}) + J^{\alpha} B(f,f_x,f_{xx}), \quad n-1 < \alpha \le n, \ t > 0.$$
(9)

## 3.1. The Zeroth-Order Deformation Equation

Let *L* denotes an auxiliary linear operator,  $f_0(x, t)$  is an initial approximation of f(x, t), satisfied by the initial condition in (8)

In (8), we have linear operator  $D_t^{\alpha}$  which in this work is different from linear operator *A* and we can choose it to be

$$L(\varphi) = D_t^{\alpha}(\varphi) \tag{10}$$

with corresponding initial approximation

$$f_0(x,t) = \sum_{k=0}^{m-1} g_k(x) \frac{t^k}{k!} + J^{\alpha} C(x,t).$$
(11)

The non-linear operator by (8) can be defined for simplicity sake as

$$N(\varphi) = D_t^{\alpha}(\varphi) - A(\varphi, \varphi_x, \varphi \varphi_{xx}) + B(\varphi, \varphi_x, \varphi_{xx}) - C(x, t).$$
(12)

We can now construct the zeroth-order deformation in the frame of Homotopy Analysis Method (HAM) [17] as

$$(1-r)L(F(x,t;r) - f_0(x,t)) = rhN(F(x,t;r)),$$
(13)

with initial conditions:

$$F^{(k)}(x,0;r) = g_k(x), \quad k = 0, 1, 2, 3, \dots, m-1.$$
 (14)

where  $h \neq 0$  is an auxiliary parameter,  $r \in [0, 1]$  is the embedding parameter and F(x, 0; r) is an unknown function on the independent variables x, t, and r.

We observe that  $\varphi = 0$  is a solution of  $L(\varphi) = 0$  where r = 0 since  $f_0(x, t)$  satisfies all the initial conditions (8).

So,

$$F(x,t;0) = f_0(x,t).$$
(15)

Also, the zeroth-order deformation equations (13) and (14) are equivalent to the original equations (8) provided r = 1 and

$$F(x,t;1) = f(x,t).$$
 (16)

Using r, we expand, in Taylor series, F as

$$F(x,t;r) = f_0(x,t) + \sum_{m=1}^{\infty} f_m(x,t)r^m.$$
(17)

where

$$f_m(x,t) = \frac{1}{m!} \left. \frac{\partial^m F(x,t;r)}{\partial r^m} \right|_{r=0}.$$
 (18)

If we assume that the auxiliary linear operator *L*, the initial guess  $f_0$  and the auxiliary parameter *h* are properly chosen such that the series (18) converges at r = 1, then by (16) we have

$$f(x,t) = f_0(x,t) + \sum_{m=1}^{\infty} f_m(x,t).$$
(19)

## 3.2. The mth-Order Deformation Equation

We consider the vector

$$\vec{f}_m = \{f_0(x,t), f_1(x,t), \dots, f_m(x,t)\}.$$
(20)

Differentiating (13) *m* times with respect to the (embedding) parameter *r*, then evaluating at r = 0 and finally dividing them by *m*!, we have the so called mth-order deformation equation (Lioa [16, 17]) as

$$L[f_m(x,t) - \chi_m f_{m-1}(x,t)] = h \mathscr{R}_m(\vec{f}_{m-1}), \qquad (21)$$

with initial conditions

$$f_m^{(k)}(x,0) = 0, \quad k = 0, 1, 2, ..., m-1.$$
 (22)

where

$$\mathscr{R}_m\left(\vec{f}_{m-1}\right) = \frac{1}{(m-1)!} \left. \frac{\partial^{m-1} N(F(x,t))}{\partial r^{m-1}} \right|_{r=0}$$
(23)

and

$$\chi_m = \begin{cases} 0 & m \le 1 \\ 1 & m > 1, \end{cases}$$
(24)

When we substitute (12) into (23), since A is a linear operator we get

$$\mathscr{R}_{m}(\vec{f}_{m-1}) = D_{t}^{\alpha} - A(f_{(m-1)}, f_{(m-1)x}, f_{(m-1)xx})$$

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$$-\frac{1}{(m-1)!} \left. \frac{\partial^{m-1} B(F, F_x, F_{xx})}{\partial r^{m-1}} \right|_{r=0} - (1 - \chi_m) C(x, t)$$
(25)

According to (10),  $J^{\alpha}$  can be applied to both sides of (21) to get

$$J^{\alpha}D^{\alpha}\left[f_{m}(x,t)-\chi_{m}f_{m-1}(x,t)\right]=hJ^{\alpha}\left[\mathscr{R}_{m}\left(\vec{f}_{m-1}\right)\right].$$
(26)

Combining property (5) and the initial conditions in (22), we have

$$f_m(x,t) = \chi_m f_{m-1}(x,t) + h J^{\alpha} \big[ \mathscr{R}_m \big( \vec{f}_{m-1} \big) \big].$$
(27)

And, finally we will approximate the HAM solution (19) for the purpose of computation by truncated series

$$\varphi_m(x,t) = \sum_{k=0}^{m-1} f_k(x,t).$$
(28)

Lemma 3 ([3]). Suppose the series

$$f(x,t) = f_0(x,t) + \sum_{m=1}^{\infty} f_m(x,t)$$

converges, where  $f_m(x, t)$  is governed by (21) with definitions (23) and (24).

Then f must be a solution of (8).

#### 3.3. Mathematical Analysis

Considering a finite cylindrical piece of homogeneous porous matrix which is saturated with native liquid *A* surrounded completely by an impermeable surface except for an end of the cylinder labelled as the imbibition face x = 0. This end is opened to an adjacent formation of injected liquid *B*, see Diagram 1. The phenomenon of fingering will occur simultaneously with imbibition for a less viscous and preferentially wetting phase of liquid *B* which describes a one-dimensional fingero-imbibition phenomena for which the injection is started by imbibition and resulting displacement produce instabilities.

We assume that the validity of Darcy's law for the double phase flow system [22] the seepage velocities of wetting phase  $(v_w)$  and the non-wetting  $(v_0)$  as:

$$\begin{cases} v_w = -\frac{k_w}{\mu_w} K \frac{\partial P_w}{\partial x} \\ v_0 = -\frac{k_0}{\mu_0} K \frac{\partial P_0}{\partial x}, \end{cases}$$
(29)

where  $k_w$ ,  $k_0$  are relative permeability,  $P_w$ ,  $P_0$  are pressure and  $\mu_w$ ,  $\mu_0$  are kinematic viscosities (constant) of wetting phase and non-wetting phase respectively and the permeability of homogeneous medium is *K*. The coordinate *x* is measured along the axis of the cylindrical medium, the origin being located at the imbibition face x = 0.

We have that

$$v_w = -v_0 \tag{30}$$

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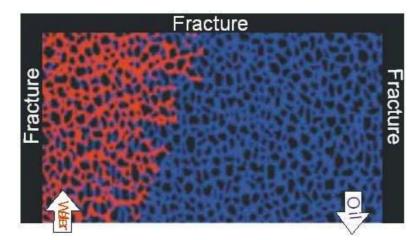


Figure 1: The Fingero-Imbibition (counter-current) Phenomena in Fractured Reservoir.

for a counter current flow.

Hence, (29) give

$$\frac{k_w}{\mu_w} K \frac{\partial P_w}{\partial x} + \frac{k_0}{\mu_0} K \frac{\partial P_0}{\partial x} = 0$$
(31)

Mehta [18], gives the definition of capillary pressure  $P_c$  as

$$P_c = P_0 - P_w \tag{32}$$

That is

$$\frac{\partial P_c}{\partial x} = \frac{\partial P_0}{\partial x} - \frac{\partial P_w}{\partial x}$$
(33)

Then (31) and (33) give

$$\left(\frac{k_w}{\mu_w} + \frac{k_0}{\mu_0}\right)\frac{\partial P_w}{\partial x} + \frac{k_0}{\mu_0}\frac{\partial P_c}{\partial x} = 0$$
(34)

From here, using (34), we can write (29) explicitly as

$$v_{w} = K\left(\frac{k_{w}}{\mu_{w}}\right)\left(\frac{k_{0}}{\mu_{0}}\right)\frac{\partial P_{c}}{\partial x}\left(\frac{k_{w}}{\mu_{w}} + \frac{\partial k_{0}}{\partial \mu_{0}}\right)^{-1}$$
(35)

For wetting phase, equation of continuity is given by

$$\phi \frac{\partial S_w}{\partial t} + \frac{\partial v_w}{\partial x} = 0 \tag{36}$$

where  $S_w$  is the saturation of the wetting phase and  $\phi$  is the porosity of the medium.

Substituting the value of  $v_w$  of (35) into (36), we obtain

$$\phi \frac{\partial S_w}{\partial t} + \frac{\partial}{\partial x} \left[ K \frac{k_w k_0}{k_w \mu_0 + k_0 \mu_w} \frac{\partial P_c}{\partial x} \right] = 0$$
(37)

Equation (37) is a non-linear partial differential equation that describes that the fingeroimbibition phenomenon of two immiscible fluids flow through homogeneous porous cylindrical medium with impervious bounding surface on three sides.

We assume standard forms of (Scheidagger and Johnson [22]) for the analytical relationship between the relative permeability, phase saturation and capillary pressure phase saturation knowing that fictitious relative permeability is the function of displacing fluid saturation.

$$k_0 = 1 - \xi S_w, \tag{38}$$

where  $\xi = 1.11$ 

$$k_w = S_w \tag{39}$$

$$P_c = \beta S_w \tag{40}$$

The model we are considering involves water and viscous oil and so according to (Scheidegger [22]), we have

$$\frac{k_0 k_w}{k_w \mu_0 + k_0 \mu_w} \approx \frac{k_0}{\mu_0} = \frac{1 - \xi S_w}{\mu_0} = \frac{S}{\mu_0}, \text{ where } S = 1 - \xi S_w.$$
(41)

Hence, by substituting (41), (40), (39), and (38) into (37), we arrived at

$$\frac{\partial S_w}{\partial t} = \frac{k\beta}{\mu_0 \phi} \frac{\partial}{\partial x} \left[ (1 - \xi S_w) \frac{\partial S_w}{\partial x} \right]$$
(42)

For a dimensionless form of (42), we choose the following new variables

$$X = \frac{x}{L} \text{ and } T = \frac{k\beta}{\phi\mu_0 L^2}t$$
(43)

to get

$$\begin{cases} \frac{\partial S_w}{\partial T} = \frac{\partial}{\partial X} \left[ (1 - \xi S_w) \frac{\partial S_w}{\partial X} \right] \\ S_w(X, 0) = f(X) = e^{-X}. \end{cases}$$
(44)

The choice of initial condition is due to the fact that the saturation of injected water decreases exponentially when x increases (Mehta [18]).

Equation (44) with  $S = 1 - \xi S_w$ , gives

$$\begin{cases} \frac{\partial S}{\partial T} = \frac{\partial}{\partial X} \left[ S \frac{\partial S}{\partial X} \right] \\ S(X,0) = f(X) = 1 - \xi e^{-X}. \end{cases}$$
(45)

## 3.4. Main Result

This present paper considers the fingero-imbibition phenomena of time-fractional type ( $\alpha > 0$  order) through porous media using HAM to obtain analytical solution

$$\begin{cases} D_T^{\alpha} S = \frac{\partial}{\partial X} \left[ S \frac{\partial S}{\partial X} \right] \\ S(X,0) = f(X) = 1 - \xi e^{-X}. \end{cases}$$
(46)

When  $\alpha = 1$ , we obtain (45) the usual fingero-imbibition phenomena through porous media. Equation (46) can be written as in (1)

$$D_T^{\alpha}S(X,T) = \left[\frac{\partial S(X,T)}{\partial X}\right]^2 + S(X,T)\frac{\partial^2 S(X,T)}{\partial X^2}$$
(47)

We construct zeroth-order deformation from (13)

.

$$\begin{cases} (1-r)L(\bar{S}(X,T;r) - \bar{S}_0(X,T)) = rhN(\bar{S}(X,T;r)) \\ \bar{S}(X,0) = f(X) = 1 - \xi e^{-X}. \end{cases}$$
(48)

where

$$N(\psi) = D_T^{\alpha} \psi - \psi_x^2 - \psi \psi_{xx}$$
<sup>(49)</sup>

The auxiliary linear operator can be chosen as

$$L(\psi) = D_T^{\alpha} \psi \tag{50}$$

with property

$$L(\psi) = 0 \text{ for } \psi = 0.$$
 (51)

While the initial guess is

$$S_0(X,T) = 1 - \xi e^{-X}.$$
 (52)

The high-order deformation equation from (21) as

$$\begin{cases} L\left[S_m(X,T) - \chi_m S_{(m-1)}(X,T)\right] = h \mathscr{R}_m\left[\vec{S}_{(m-1)}(X,T)\right] \\ S_m^{(k)}(X,0) = 0, \quad k = 0, 1, \end{cases}$$
(53)

where

$$\mathscr{R}_{m}\left[\vec{S}_{(m-1)}\right] = \frac{1}{(m-1)!} \left. \frac{\partial^{m-1}N\left[S(X,T;r)\right]}{\partial r^{m-1}} \right|_{r=0}$$
(54)

Then,  $\mathscr{R}_m \left[ \vec{S}_{(m-1)} \right]$  can be given by

$$\mathscr{R}_{m}\left[\vec{S}_{(m-1)}\right] = D_{T}^{\alpha}S_{(m-1)} - \sum_{i=0}^{m-1} S_{ix}S_{(m-1-i)x} - \sum_{i=0}^{m-1} S_{i}S_{(m-1-i)xx}$$
(55)

Accordingly, the governing equation is as follows:

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$$S_m = \chi_m S_{m-1} + h J^{\alpha} \left[ D_T^{\alpha} S_{(m-1)} - \sum_{i=0}^{m-1} S_{ix} S_{(m-1-i)x} - \sum_{i=0}^{m-1} S_i S_{(m-1-i)xx} \right]$$
(56)

where  $m \ge 1$ .

Using (56), we obtain the first few terms of HAM series solutions as follows

$$S_0(X,T) = 1 - \xi e^{-X}, \tag{57}$$

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$$S_{1}(X,T) = \chi_{1}S_{0} + hJ^{\alpha} \begin{bmatrix} {}^{C}D_{T}^{\alpha}S_{0} - S_{0x}^{2} - S_{0}S_{0xx} \end{bmatrix}$$
  
=  $-hJ^{\alpha} \left( 2\xi^{2}e^{-2X} - \xi e^{-X} \right)$   
=  $-2h\xi^{2}e^{-2X}\frac{T^{\alpha}}{\Gamma(\alpha+1)} + h\xi e^{-X}\frac{T^{\alpha}}{\Gamma(\alpha+1)},$  (58)

$$S_{2}(X,T) = \chi_{2}S_{1} + hJ^{\alpha} \Big[ {}^{C}D_{T}^{\alpha}S_{1} - 2S_{0x}S_{1x} - S_{0}S_{1xx} - S_{1}S_{0xx} \Big]$$
  
$$= -2h\xi^{2}e^{-2X}\frac{T^{\alpha}}{\Gamma(\alpha+1)} + h\xi e^{-X}\frac{T^{\alpha}}{\Gamma(\alpha+1)} - 2h^{2}\xi^{2}e^{-2X}\frac{T^{\alpha}}{\Gamma(\alpha+1)}$$
  
$$+ h^{2}\xi e^{-X}\frac{T^{\alpha}}{\Gamma(\alpha+1)} + 12h^{2}\xi^{2}e^{-2X}\frac{T^{2\alpha}}{\Gamma(2\alpha+1)}$$
  
$$- 18h^{2}\xi^{3}e^{-3X}\frac{T^{2\alpha}}{\Gamma(2\alpha+1)} - h^{2}\xi e^{-X}\frac{T^{2\alpha}}{\Gamma(2\alpha+1)}.$$
 (59)

The remaining terms for m = 3, 4, ... can be obtained using Mathematica or MATLAB

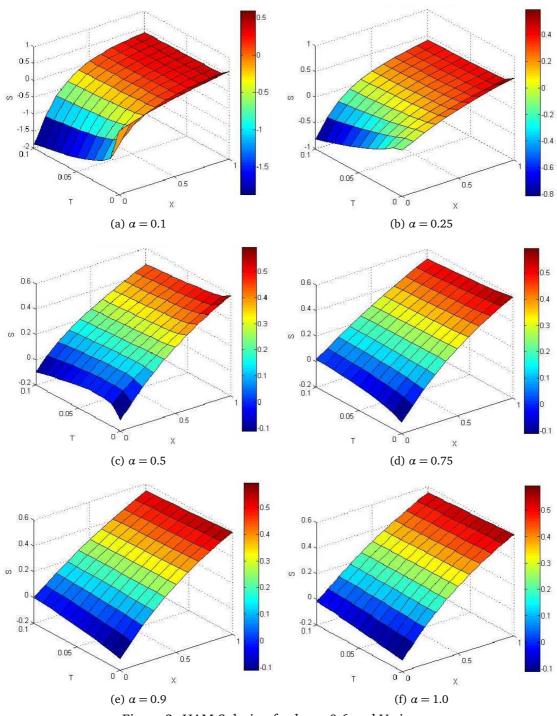
Hence, the HAM series solution is obtained as

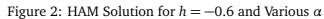
$$S(X,T) = S_0(X,T) + S_1(X,T) + S_2(X,T) + S_3(X,T) + \dots$$
  
=  $1 - \xi e^{-X} - 4h\xi^2 e^{-2X} \frac{T^{\alpha}}{\Gamma(\alpha+1)} + 2h\xi e^{-X} \frac{T^{\alpha}}{\Gamma(\alpha+1)}$   
 $- 2h^2 \xi^2 e^{-2X} \frac{T^{\alpha}}{\Gamma(\alpha+1)} + h^2 \xi e^{-X} \frac{T^{\alpha}}{\Gamma(\alpha+1)} + 12h^2 \xi^2 e^{-2X} \frac{T^{2\alpha}}{\Gamma(2\alpha+1)}$   
 $- 18h^2 \xi^3 e^{-3X} \frac{T^{2\alpha}}{\Gamma(2\alpha+1)} - h^2 \xi e^{-X} \frac{T^{2\alpha}}{\Gamma(2\alpha+1)} + \dots$  (60)

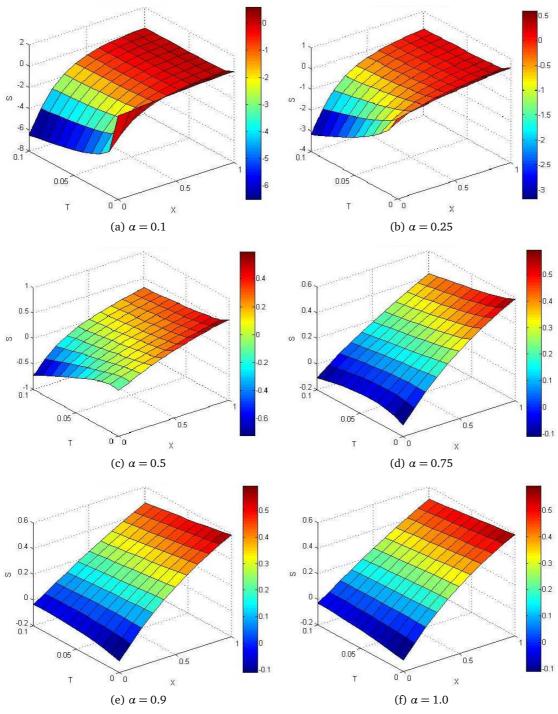
Table 1 shows the few terms HAM approximation of (1) when  $\alpha = 0.10, 0.25, 0.50, 0.75, 0.90$ and 1.00 with h = -0.6 and -1.0 and their respective solution plots by Matlab are given in Figures 2-3. Curves representing the effect of different values of h on the saturation S for fixed T and  $\alpha$  are shown in Figures 4-5; Figure 6 represents the effect of different values of  $\alpha$  on the saturation for fixed T and h.

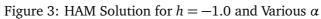
		$\alpha = 0.10$			$\alpha = 0.25$		$\alpha = 0.50$		$\alpha = 0.75$		$\alpha = 0.90$		$\alpha = 1.00$	
Т	X	h = -0.6	h = -1.0	h = -0.6	h = -1.0		h = -1.0	h = -0.6	h = -1.0	h = -0.6	h = -1.0 l	n = -0.6 l	n = -1.0	
0.02		-0.7577		-0.1072		0.0624	-0.0345		0.0213	0.0171	0.0136	0.0099	0.0083	
	0.2000	-0.4092	-2.0031	0.0119	-0.5400	0.1279	0.0350	0.1128	0.0939	0.1037	0.0954	0.0995	0.0946	
	0.3000	-0.1685	-1.2864	0.1039	-0.3206	0.1898	0.0984	0.1871	0.1629	0.1833	0.1715	0.1815	0.1740	
	0.4000	-0.0010	-0.8020	0.1775	-0.1629	0.2483	0.1576	0.2560	0.2280	0.2563	0.2420	0.2563	0.2471	
	0.5000	0.1174	-0.4758	0.2389	-0.0464	0.3038	0.2133	0.3198	0.2893	0.3232	0.3073	0.3245	0.3142	
	0.6000	0.2034	-0.2559	0.2921	0.0429	0.3562	0.2663	0.3787	0.3468	0.3844	0.3676	0.3867	0.3757	
	0.7000	0.2682	-0.1063	0.3396	0.1143	0.4056	0.3168	0.4330	0.4905	0.4404	0.4231	0.4433	0.4321	
	0.8000	0.3196	-0.0022	0.3833	0.1742	0.4521	0.3650	0.4830	0.4505	0.4915	0.4741	0.4949	0.4836	
	0.9000	0.3624	0.0730	0.4240	0.2267	0.4957	0.4108	0.5289	0.4970	0.5389	0.5210	0.5418	0.5306	
	1.0000	0.4010	0.1304	0.4625	0.2743	0.5365	0.4544	0.5710	0.5400	0.5806	0.5640	0.5844	0.5736	
0.04	0.1000	-0.9102	-3.5498	-0.2189	-1.2668	0.0599	-0.1306	0.0522	0.0213	0.0334	0.0231	0.0232	0.0181	
	0.2000	-0.5073	-2.3261	-0.0613	-0.8213	0.1240	-0.0412	0.1236	0.0848	0.1131	0.0952	0.1072	0.0961	
	0.3000	-0.2308	-1.4956	0.0548	-0.5125	0.1833	0.0338	0.1911	0.1461	0.1873	0.1638	0.1848	0.1693	
	0.4000	-0.0404	-0.9360	0.1431	-0.2965	0.2388	0.0990	0.2547	0.2053	0.2561	0.2287	0.2563	0.2377	
	0.5000	0.0924	-0.5613	0.2129	-0.1431	0.2912	0.1578	0.3144	0.2621	0.3199	0.2899	0.3221	0.3014	
	0.6000	0.1868	-0.3109	0.2705	-0.0310	0.3409	0.2121	0.3702	0.3163	0.3788	0.3473	0.3825	0.3606	
	0.7000	0.2564	-0.1430	0.3200	0.0539	0.3881	0.2631	0.4223	0.3678	0.4331	0.4009	0.4378	0.4154	
	0.8000	0.3100	-0.0287	0.3642	0.1214	0.4328	0.3115	0.4707	0.4166	0.4831	0.4509	0.4885	0.4660	
	0.9000	0.3537	0.0518	0.4048	0.1779	0.4752	0.3577	0.5156	0.4625	0.5290	0.4873	0.5349	0.5127	
	1.0000	0.3914	0.1114	0.4428	0.2275	0.5152	0.4019	0.5572	0.5057	0.5711	0.5403	0.5773	0.5557	
0.06	0.1000	-1.0111	-3.8724	-0.3102	-1.5916	0.0461	-0.2376	0.0649	0.0098	0.0471	0.0270	0.0354	0.0251	
	0.2000	-0.5721	-2.5373	-0.1209	-1.0388	0.1136	-0.1205	0.1304	0.0694	0.1209	0.0918	0.1143	0.0958	
	0.3000	-0.2719	-1.6318	0.0156	-0.6585	0.1738	-0.7285	0.1930	0.1271	0.1904	0.1545	0.1878	0.1634	
	0.4000	-0.0661	-1.0227	0.1165	-0.3958	0.2289	0.0471	0.2526	0.1829	0.2556	0.2150	0.2562	0.2276	
	0.5000	0.0762	-0.6159	0.1937	-0.2126	0.2803	0.1118	0.3092	0.2370	0.3166	0.2728	0.3196	0.2883	
	0.6000	0.1764	-0.3455	0.2555	-0.0820	0.3288	0.1695	0.3626	0.2891	0.3734	0.3278	0.3783	0.3453	
	0.7000	-0.2491	-0.1655	0.3070	0.0139	0.3747	0.2222	0.4129	0.3393	0.4262	0.3799	0.4324	0.3987	
	0.8000	0.3044	-0.0443	0.3520	0.0876	0.4184	0.2717	0.4601	0.3872	0.4752	0.4290	0.4822	0.4486	
	0.9000	0.3487	0.0395	0.3927	0.1473	0.4600	0.3185	0.5042	0.4329	0.5205	0.4751	0.5281	0.4949	
	1.0000	0.3864	0.1006	0.4305	0.1984	0.4995	0.3633	0.5454	0.4762	0.5622	0.5182	0.5702	0.5380	

Table 1: HAM Approximation of (1) Varying  $\alpha$  and h









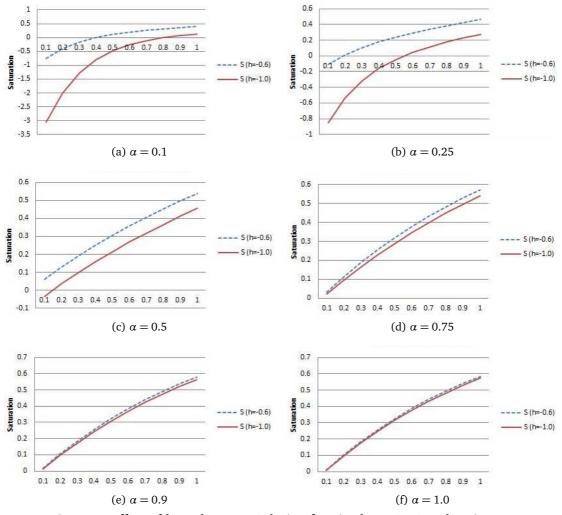


Figure 4: Effect of *h* on the HAM Solution for Fixed T = 0.02 and Various  $\alpha$ 

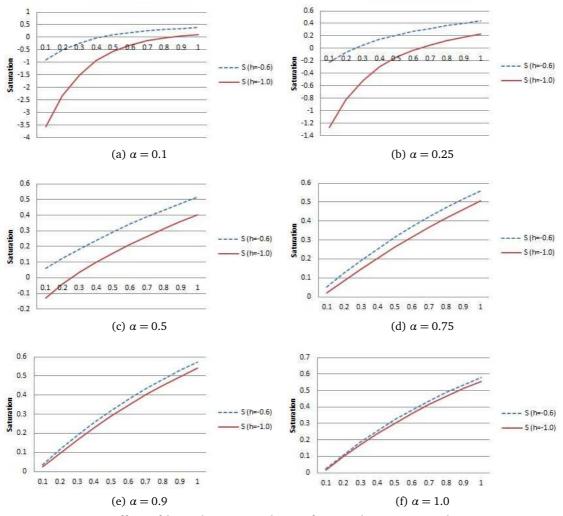


Figure 5: Effect of *h* on the HAM Solution for Fixed T = 0.04 and Various  $\alpha$ 

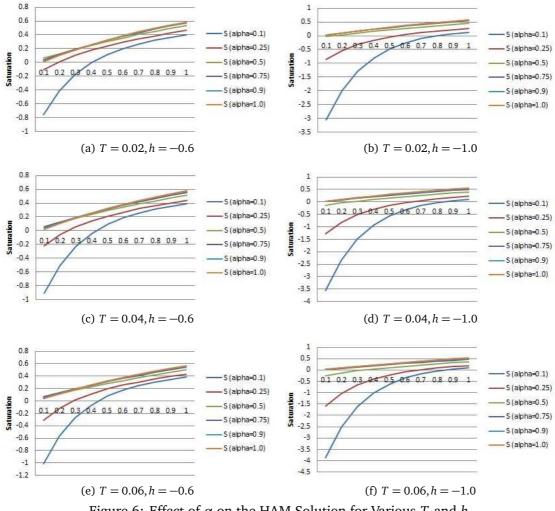


Figure 6: Effect of  $\alpha$  on the HAM Solution for Various T and h

When  $\alpha = 1$  and h = -0.03, the problem solved by [19], using Adomian Decomposition Method, *ADM*, coincides with our problem and so the solutions were compared in Table 2 and is represented in Figure 7.

	T = 0.02			T = 0.04		T = 0.06			
X	$S_{HAM}$	$S_{ADM}$	X	$S_{HAM}$	$S_{ADM}$	X	$S_{HAM}$	S <sub>ADM</sub>	
0.1000	0.0099	0.0146	0.1000	0.0232	0.0315	0.1000	0.0354	0.0471	
0.2000	0.0995	0.1052	0.1000	0.1072	0.1178	0.1000	0.1143	0.1294	
0.3000	0.1815	0.1878	0.1000	0.1848	0.1969	0.1000	0.1878	0.2053	
0.4000	0.2563	0.2629	0.1000	0.2563	0.2692	0.1000	0.2562	0.2751	
0.5000	0.3245	0.3313	0.1000	0.3221	0.3354	0.1000	0.3196	0.3392	
0.6000	0.3867	0.3834	0.1000	0.3825	0.3958	0.1000	0.3783	0.3981	
0.7000	0.4433	0.4499	0.1000	0.4378	0.4510	0.1000	0.4324	0.4520	
0.8000	0.4949	0.5012	0.1000	0.4885	0.5013	0.1000	0.4822	0.5012	
0.9000	0.5418	0.5479	0.1000	0.5349	0.5471	0.1000	0.5281	0.5464	
1.0000	0.5844	0.5902	0.1000	0.5773	0.5888	0.1000	0.5702	0.5876	

Table 2: Comparison of Solutions Using HAM vs. ADM

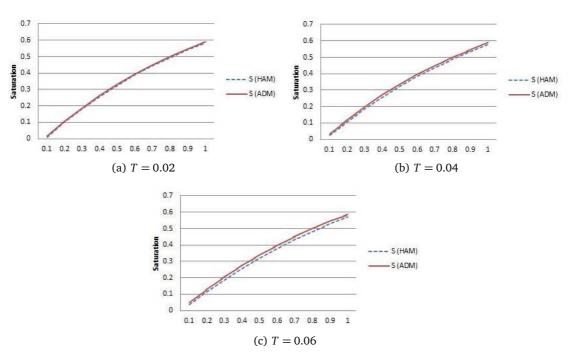


Figure 7: Comparison of HAM solution and ADM solution for Various T

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## 4. Discussion and conclusion

The basis for many scientific and engineering applications is now depending largely on the study of physics of flow through porous media. The applications ranges from hydrologist in his study of the migration of underground water, the petroleum engineer in his study of movement of oil, gas and water through the reservoir of oil or gas field, the chemical engineer in connection with filtration processes. We also have applications in soil mechanics, ceramic engineering, oil recovery process, water purification and powder metallurgy. In the recent years, Caputo [6] and He [10], fractional order have been incorporated into existing differential equations which have deep meaning and applications inexhaustible giving hope for future research work in the field of sciences and other related fields.

In this work, we propose the fractional Fingero-imbibition equation to model the spontaneous imbibition of water by an oil-saturated rock in a double phase flow through porous media. Homotopy Analysis Method (HAM) was implemented to obtain the approximate analytical solution of (1). The convergence region of the series solution obtained by HAM can be adjusted and controlled by the auxiliary parameter h such adjustments are demonstrated represented in Figures 4-5. It is interesting to note that different values  $\alpha$  have significant effect on the saturation level and so it is worth investigating. The results are shown in Figure 6.

Our results extend the work of Meher *et al.* in [19] by moving away from the classical Fingero-imbibition equation to fractional order and also using HAM (instead of ADM) which has been proven to be more accurate due to the presence of control parameter *h*. Several numerical results are presented including graphs to illustrates different scenario. Table 2 and Figures 7a-7c give the analysis of the comparison made between HAM and that of ADM in [19] when  $\alpha = 1$  and for some fixed *T* to show the efficiency and accuracy of the suggested method. The numerical simulations are obtained using MATLAB *R*2007*b* and Microsoft Excel 2010.

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